

Capacitive Protection System for Robot dedicated to the Safety of Humans

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Outline

I. Towards a model (5 slides)

- Capacitive coupling (1 slide)
- Coefficients of capacitance and induction (1 slide)
- Implementation, Modelisation and Validation (3 slides)

II. Detection and discrimination set-up (2 slides)

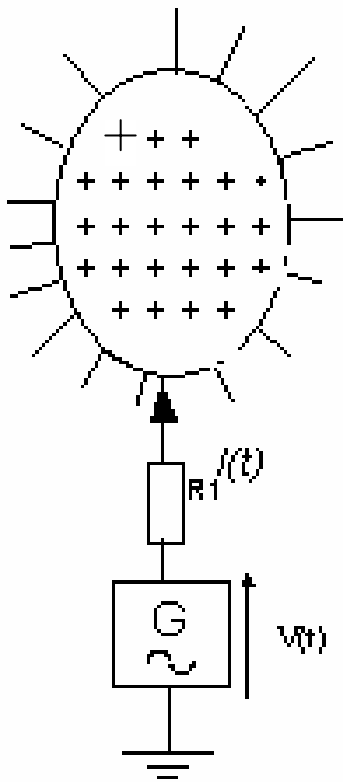
- Detection of an intruder (1 slide)
- Discrimination Human/Object and evaluation of the distance intruder/active sensor (1 slide)

III. Practical implementation and Precaution (2 slides)

IV. Conclusion

INPI (french National Institute of Intellectual Protection) under the number : 0602599 at the date 27/03/06

I. Towards a model : CAPACITIVE COUPLING

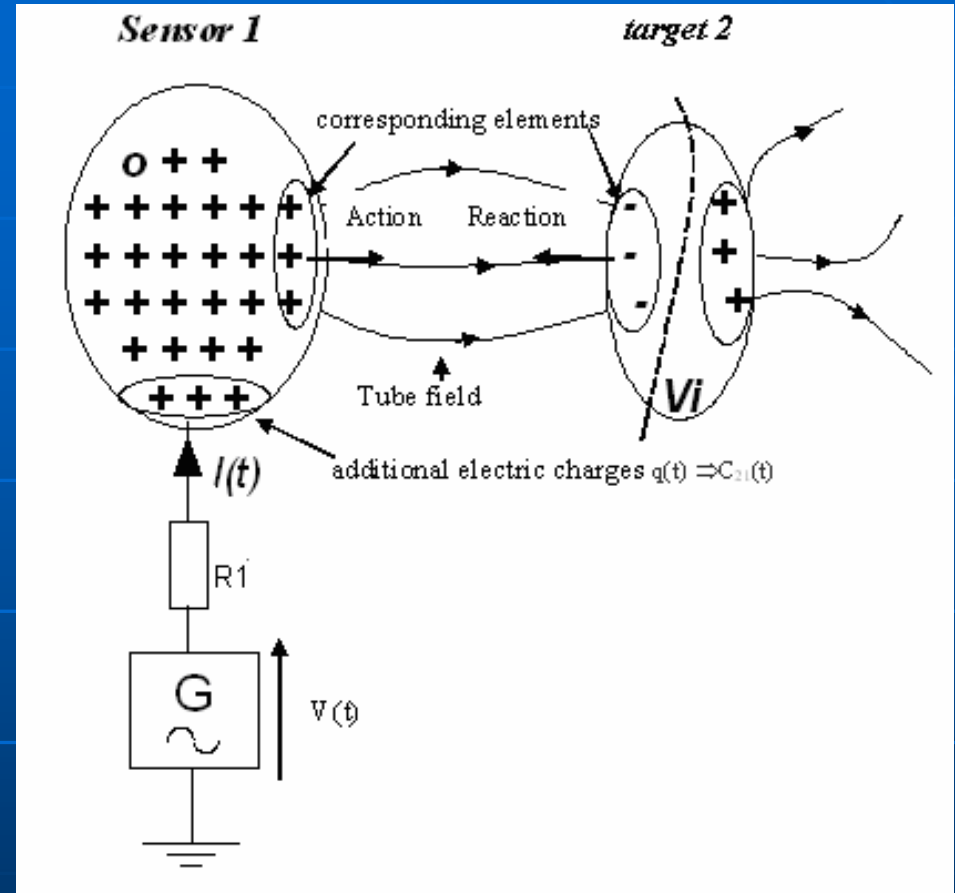


$$V(t) = V_0 \sin(2\pi ft)$$

C_{S0} : coefficient of capacitance of a sensor without target.

$$C_{S0} = \frac{Q(t)}{V(t)}$$

C_{11} : coefficient of capacitance of a 'sensor 1' in front of a target.



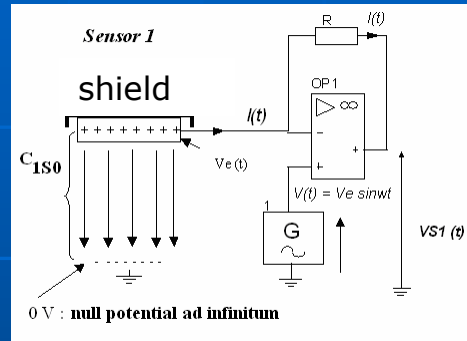
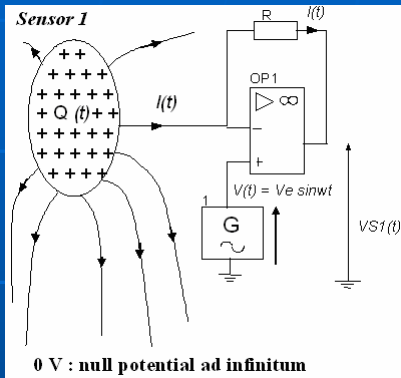
$$C_{11}(t) = \frac{Q(t) + q(t)}{V(t)} = C_{1S}(\dots) + C_{21}(t) \quad C_{1S}(\dots) = C_{11}(t) - C_{21}(t)$$

C_{1S} is the coefficient of capacitance of the sensor

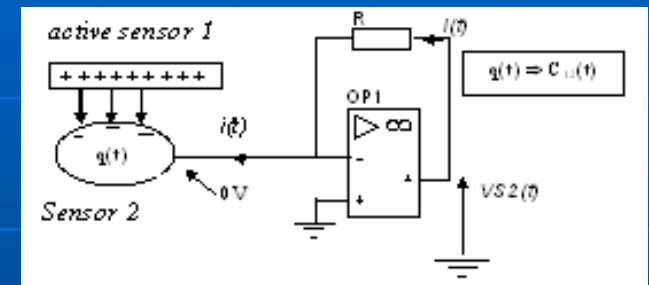
$C_{21} = C_{12}$ is the coefficient of induction of a target on the 'sensor 1'.

I. Towards a model : COEFFICIENTS OF CAPACITANCE AND INDUCTION How to measure ?

Capacitance C_{11}

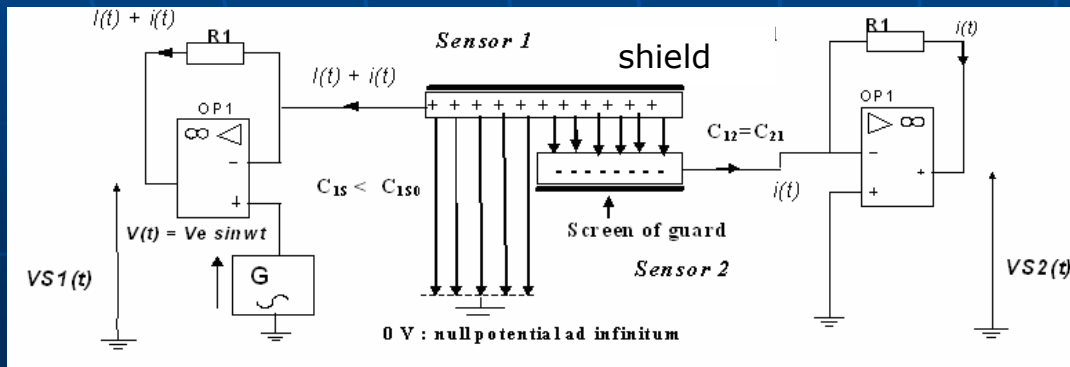


Capacitance C_{12}



Model (1) $V_{S1} = V_e \sqrt{1 + [R\omega C_{11}]^2} = V_e \sqrt{1 + (R\omega)^2 [C_{1S(\dots)} + C_{21}]^2}$

Model (2) $V_{S2} = V_e R \omega C_{12}$



$$C_{11} = C_{1S(\dots)} + C_{21} = \frac{I}{V_e R \omega} \sqrt{V_{S1}^2 - V_e^2}$$

$$C_{12} = C_{21} = \frac{I}{V_e R \omega} V_{S2}$$

I. Towards a model : MODELLISATION, IMPLEMENTATION and VALIDATION (1/3)

Theoretical model (3) : from eq(1) and eq(2)

$$\text{Eq(1)} \quad C_{11} = C_{1S}(\dots) + C_{21} = \frac{l}{V_e R \omega} \sqrt{V_{S1}^2 - V_e^2}$$

$$\text{Eq(2)} \quad C_{12} = C_{21} = \frac{l}{V_e R \omega} V_{S2}$$

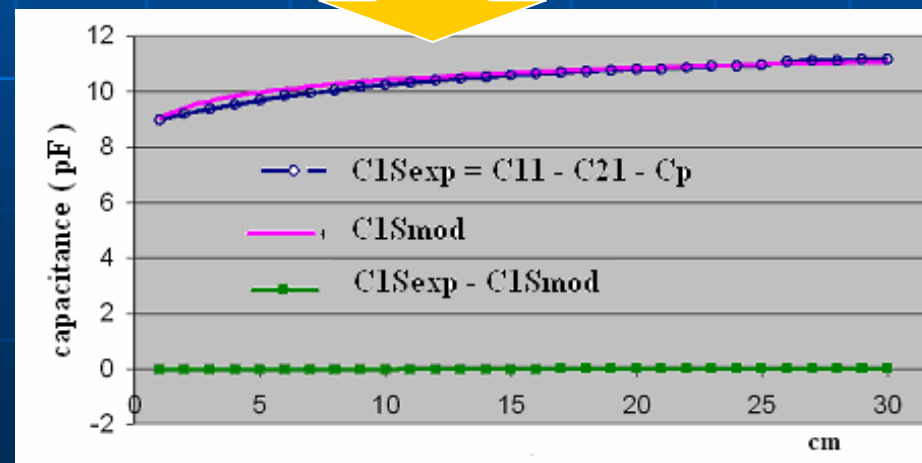
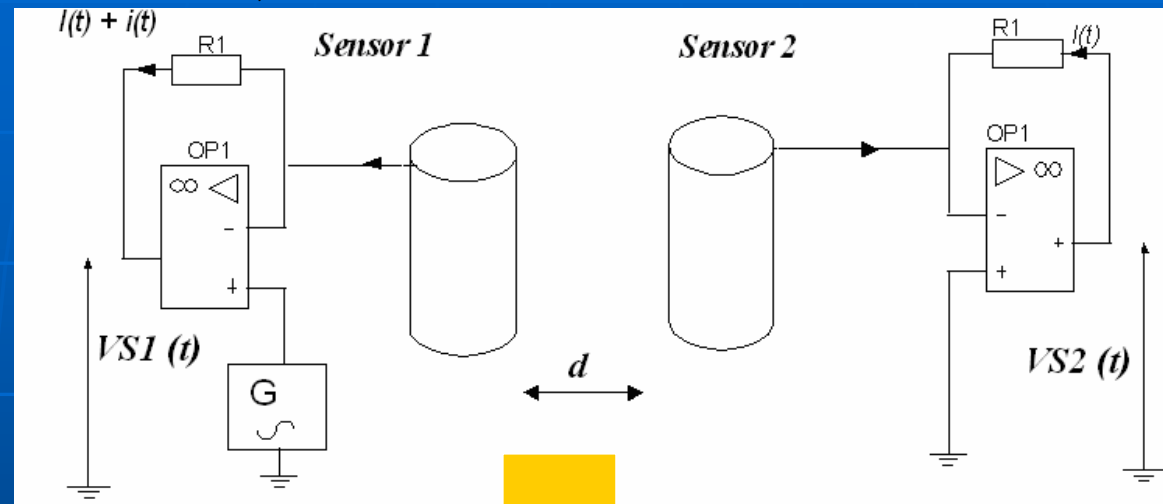
$$\text{Mod(3)} \quad C_{1S}(\dots)_{\text{exp}} = C_{11} - C_{21} = \frac{1}{V_e R \omega} \left(\sqrt{V_{S1}^2 - V_e^2} - V_{S2} \right)$$

Reference model (4) : experimentally established

$$\text{Mod(4)} \quad C_{1S}(\dots)_{\text{modl}} = C_{1S0} \left[1 - \frac{C_{21}^\alpha}{C_{1S0} + C_{21}} \right] \text{ with } \alpha = \frac{C_{1S0} + \beta C_{21}}{C_{1S0}}$$

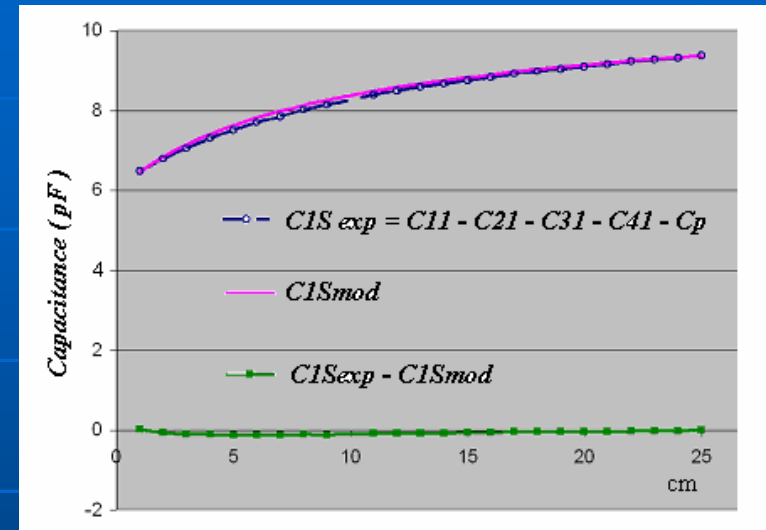
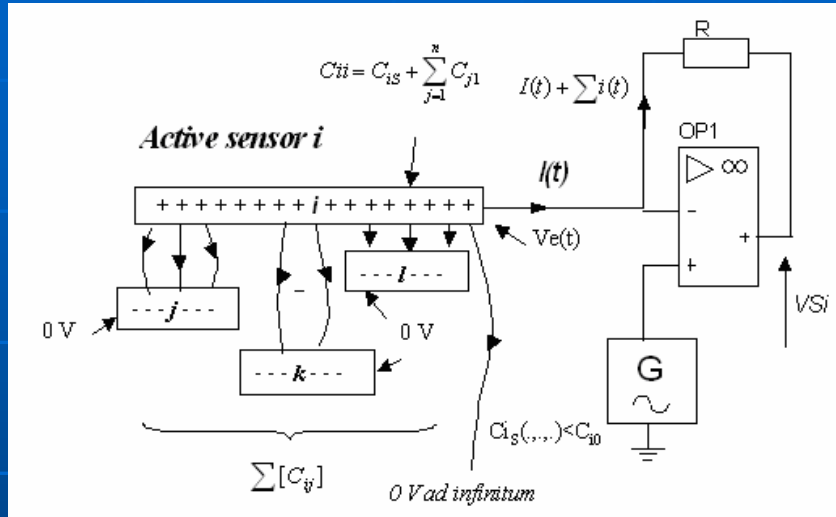
where β is an empirical variable of adjustment.
 available $3\text{mm} < d < 500\text{mm}$

I. Towards a model : MODELISATION, IMPLEMENTATION and VALIDATION (2/3)



Model
Validation
 $\beta = 1$

I. Towards a model : MODELLISATION, IMPLEMENTATION and VALIDATION (3/3) Generalization: one active 'sensor i' and n-1 inactive sensors



Translation of the coupling for n passive sensors

Validation of the models $\beta = 1$

Reference model (5) :

$$C_{is(.,.,.)_{ref}} = C_{is0} \left[1 - \frac{\sum_{j=1, i \neq j}^n C_{ji}^\alpha}{C_{is0} + \sum_{j=1, i \neq j}^n C_{ji}} \right], \quad \alpha = \frac{C_{is0} + \beta \sum_{j=1, i \neq j}^n C_{ji}}{C_{is0}}$$

Experimental model (6) :

$$C_{is(.,.,.)_{exp}} = C_{ii} - \sum_{j=1, i \neq j}^n C_{ji} = \frac{1}{V_e R \omega} \left(\sqrt{V_{Si}^2 - V_e^2} - \sum_{j=1, i \neq j}^n V_{Sj} \right)$$

Outline

I. Towards a model (5 slides)

- Capacitive coupling
- Coefficients of capacitance and induction
- Modelisation, Implementation and Validation

II. Detection and discrimination set-up (2 slides)

- Detection of an intruder (1 slide)
- Discrimination Human/Object and evaluation of the distance intruder/active sensor (1 slide)

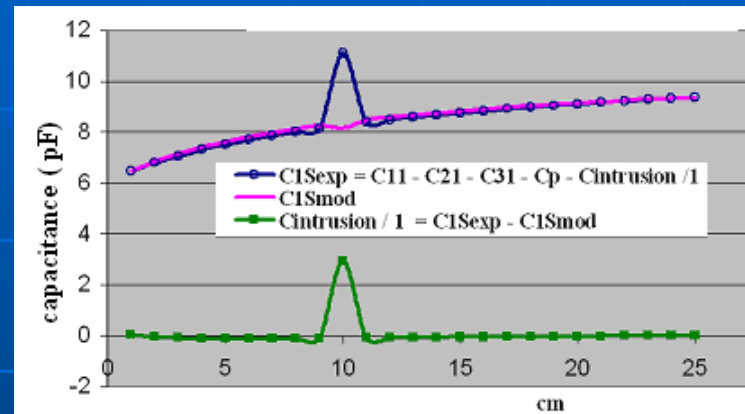
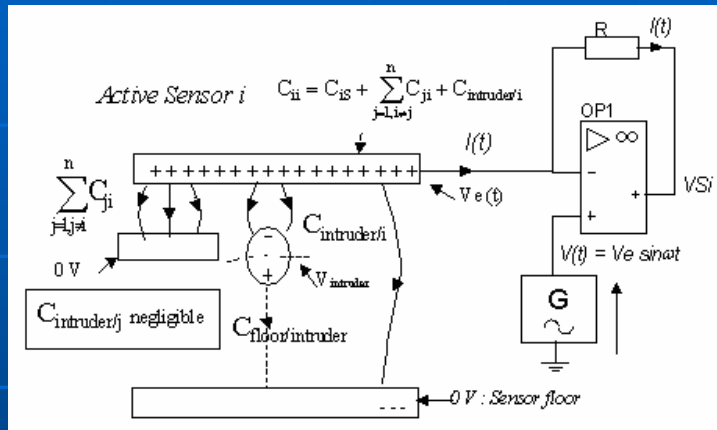
III. Practical implementation and Precaution (2 slides)

IV. Conclusion

INPI (National institute of intellectual protection) under the number : 0602599 at the date 27/03/06

II. Detection and Discrimination Set-up: DETECTION OF AN INTRUDER AND VALIDATION

A. The intruder is **not in contact** with the floor (far enough), this latter behaves like a 'sensor j' at a null potential



By measuring the potential at the output of the circuit

Reference model

$$V_{Si} = V_e \sqrt{1 + (R\omega)^2 [C_{iS} + \sum_{j=1, i \neq j}^n C_{ji} + C_{intruder/i}]^2}$$

$$\sum_{j=1, i \neq j}^n V_{Sj} = V_e \cdot R\omega [\sum_{j=1, i \neq j}^n C_{ij} + C_{intruder/j}] \approx V_e R\omega \sum_{j=1, i \neq j}^n C_{ij}$$



$$C_{intruder/i} = C_{iS}(\dots)_{exp} - C_{iS}(\dots)_{ref}$$

B. The intruder is **in contact** with the floor, the capacitive coupling intruder/floor is not negligible.

$$C_{intruder/i} = C_{iS}(\dots)_{exp} - C_{iS}(\dots)_{ref} - C_{intruder/floor}$$

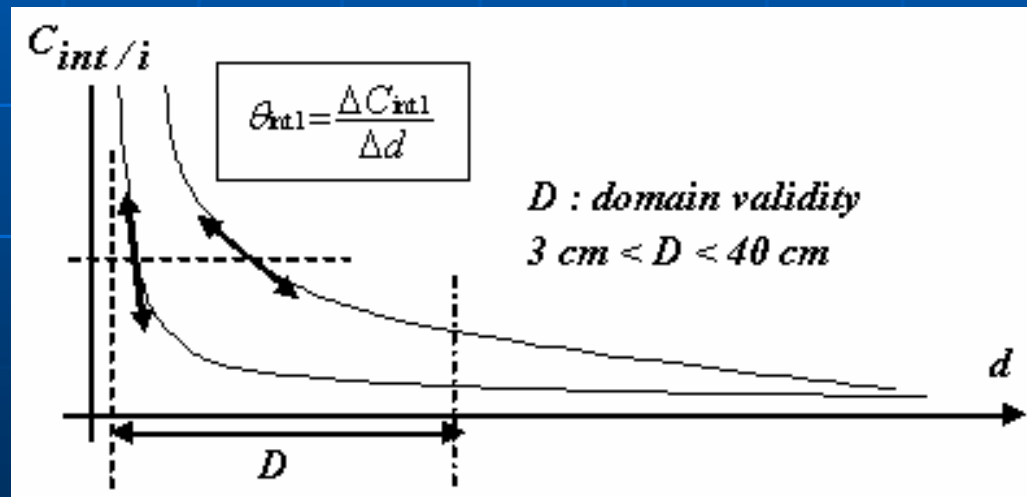
II Detection and Discrimination Set-up : DISCRIMINATION human/object Evaluation of the distance intruder/active sensor

The Coefficient of induction is modelled by: $C_{inti} = \epsilon \frac{S}{d_i}$

$$\theta_{inti} = \frac{\Delta C_{inti}}{\Delta d} = \frac{C_{inti}(d_i + \Delta d) - C_{inti}(d_i)}{\Delta d}$$

$$\theta_{inti} = \frac{\epsilon S}{\Delta d} \left[\frac{1}{d_i + \Delta d} - \frac{1}{d_i} \right] \approx -\frac{\epsilon S}{d_i^2}$$

$$\left| \frac{C_{int/i}}{\theta_{int/i}} \right| = d_i \Rightarrow \epsilon S$$



Localization and discrimination of the intruder

Outline

I. Towards a model (5 slides)

- Capacitive coupling
- Coefficients of capacitance and induction
- Implementation and Validation

II. Detection and discrimination set-up (2 slides)

- Detection of an intruder
- Discrimination Human/Object and evaluation of the distance intruder/active sensor

III. Practical implementation and Precaution (2 slides)

IV. Conclusion

INPI (National institute of intellectual protection) under the number : 0602599 at the date 27/03/06

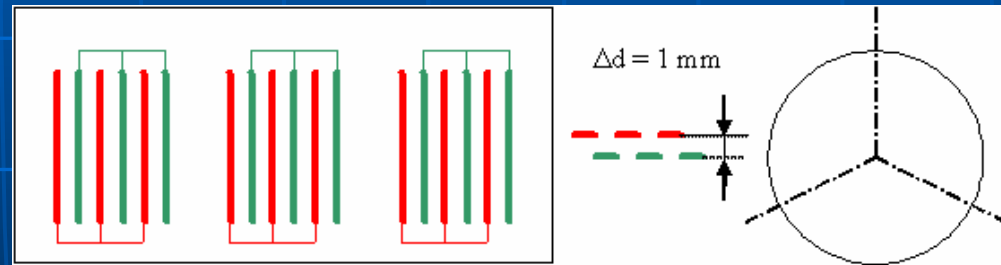
III. PRACTICAL IMPLEMENTATION AND PRECAUTION (1/2)

A. Sensor protection against parasites generated by the robot itself (*electric motor, coders of position, power supply*)

- 1st layer : conducting paint at 0Volt
- 2nd layer : isolating paint
- 3rd layer : conducting paint which is a sensor of the safety device

Consequently

- The geometry is adaptable
- The sensor is orientable
- The weight is negligible
- The space hindrance is negligible
- The sensor is cheap



III. PRACTICAL IMPLEMENTATION AND PRECAUTION (2/2)

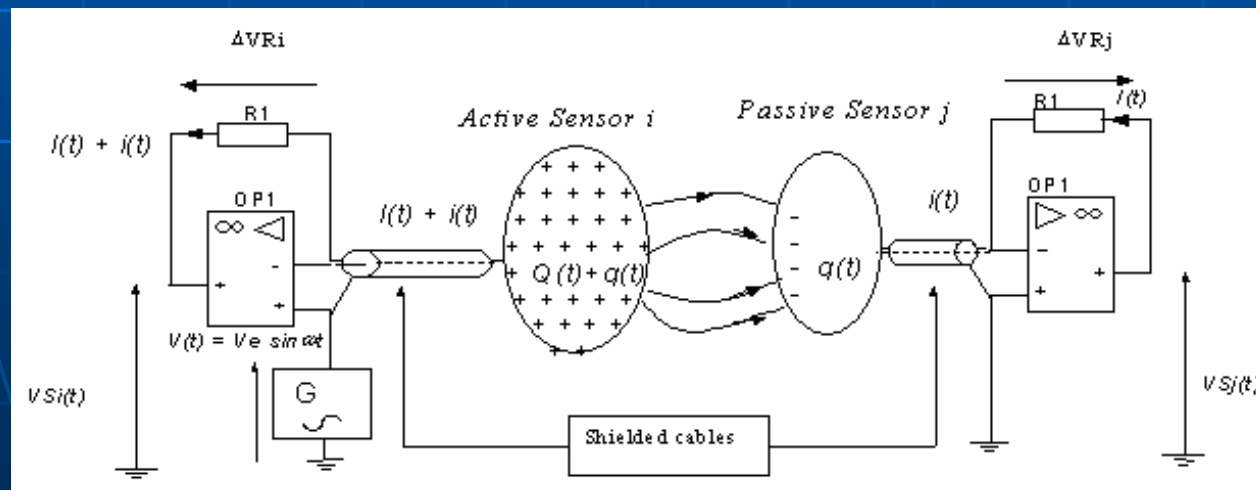
B. Sensor connection to an integrated linear amplifier :

Simple electric wire behaves like a sensor

- inverting input welded on the sensor
- shielded cable,

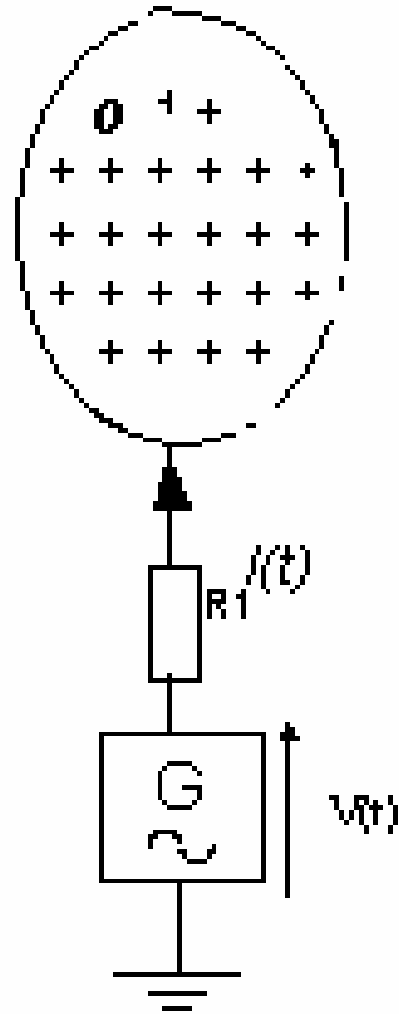
the wire is connected to the inverting input

the shielding is connected to the non inverting input

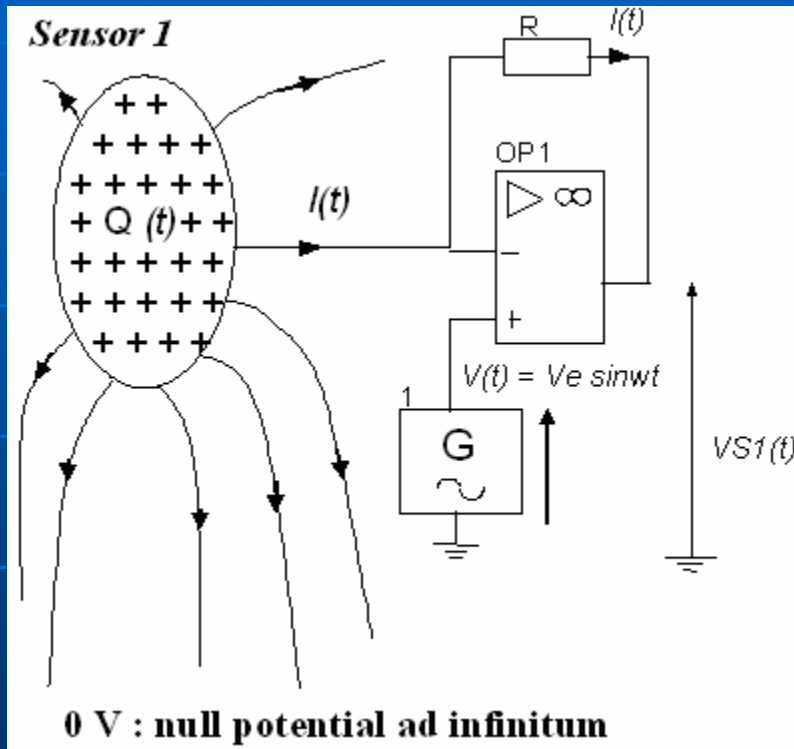


IV. CONCLUSION

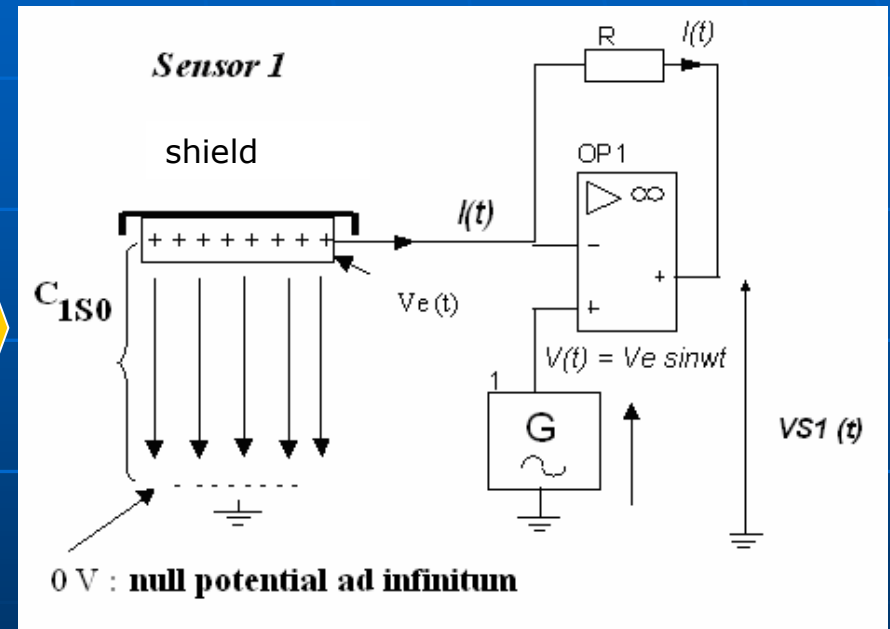
- The set-up is dedicated to safety of people working on automated sites of production.
- It lies on capacitive coupling between a sensor and a target.
- It makes it possible :
 - to detect the presence of an intruder in its environment,
 - to discriminate the nature of the intruder
 - to appreciate the distance of it.
- Industries using automated workshops of production should be interested in this type of safeguarding device.
- It is protected by a french patent to the INPI (National institute of intellectual protection) under the number : 0602599 at the date 27/03/06 .



I. Towards a model :
COEFFICIENTS OF CAPACITANCE AND INDUCTION (1/2)
 How to measure ?



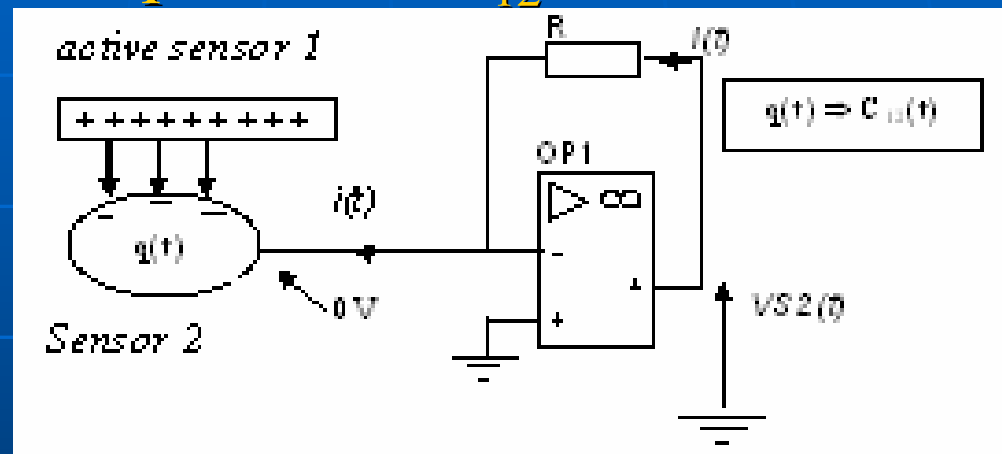
Capacitance C_{11}



$$\text{Model (1)} \quad V_{S1} = V_e \sqrt{1 + [R\omega C_{11}]^2} = V_e \sqrt{1 + (R\omega)^2 [C_{1S}(\dots) + C_{21}]^2}$$

I. Towards a model :
 COEFFICIENTS OF CAPACITANCE AND INDUCTION (2/2)
 How to measure ?

Capacitance C_{12}



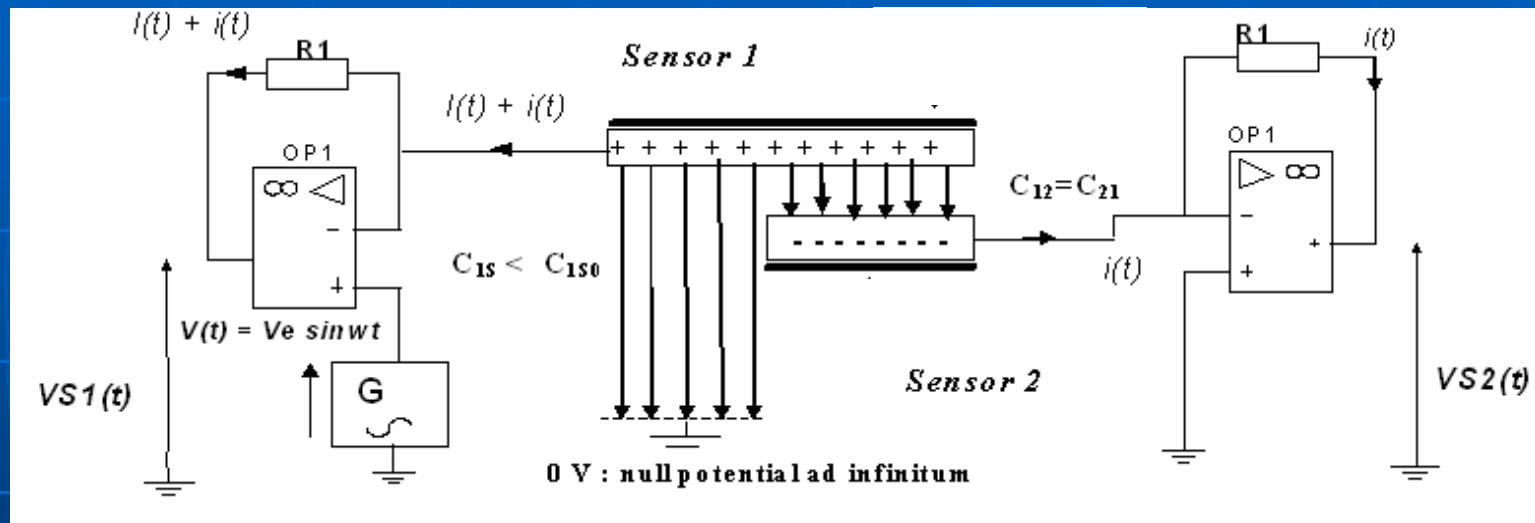
The electric potential $V_{S2}(t)$ gives us access to C_{12}

Model (2) : $V_{S2} = V_e R \omega C_{12}$

I. Towards a model : IMPLEMENTATION, MODELISATION and VALIDATION (1/4)

A. An active 'sensor 1', a 'sensor 2' at a null potential

2 arms
of a
robot



$$\text{Model (1)} \Rightarrow C_{11} = C_{1s}(\dots) + C_{21} = \frac{1}{V_e R \omega} \sqrt{V_{S1}^2 - V_e^2}$$

$$\text{Model (2)} \Rightarrow C_{12} = C_{21} = \frac{1}{V_e R \omega} V_{S2}$$

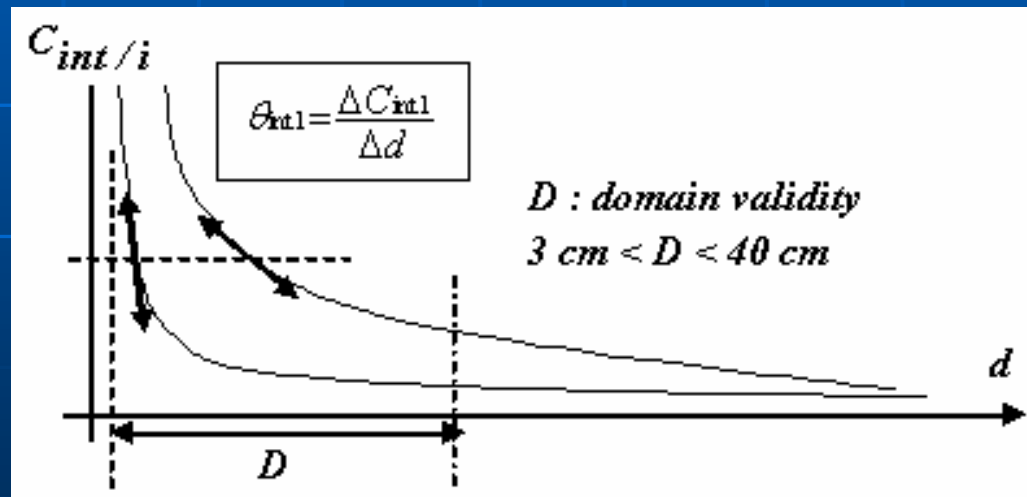
II Detection and Discrimination Set-up : DISCRIMINATION human/object Evaluation of the distance intruder/active sensor

The Coefficient of induction is modelled by: $C_{inti} = \epsilon \frac{S}{d_i}$

$$\theta_{inti} = \frac{\Delta C_{inti}}{\Delta d} = \frac{C_{inti}(d_i + \Delta d) - C_{inti}(d_i)}{\Delta d}$$

$$\theta_{inti} = \frac{\epsilon S}{\Delta d} \left[\frac{1}{d_i + \Delta d} - \frac{1}{d_i} \right] \approx -\frac{\epsilon S}{d_i^2}$$

$$\left| \frac{C_{int/i}}{\theta_{int/i}} \right| = d_i \Rightarrow \epsilon S$$



Localization and discrimination of the intruder

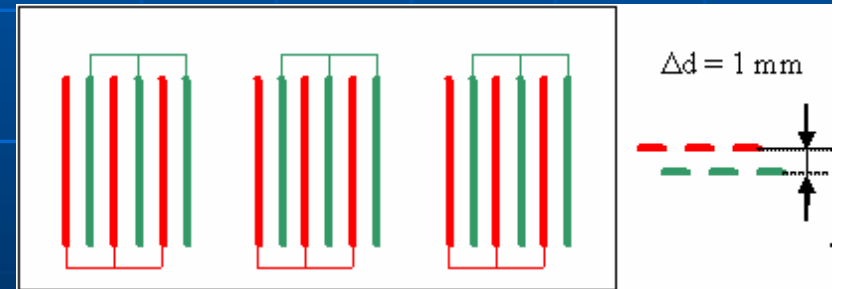
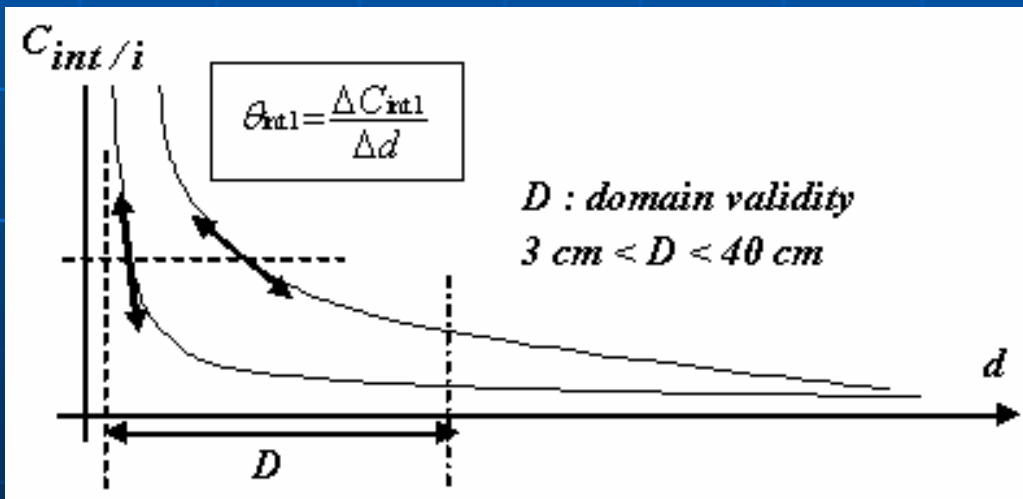
II Detection and Discrimination Set-up : DISCRIMINATION human/object Evaluation of the distance intruder/active sensor

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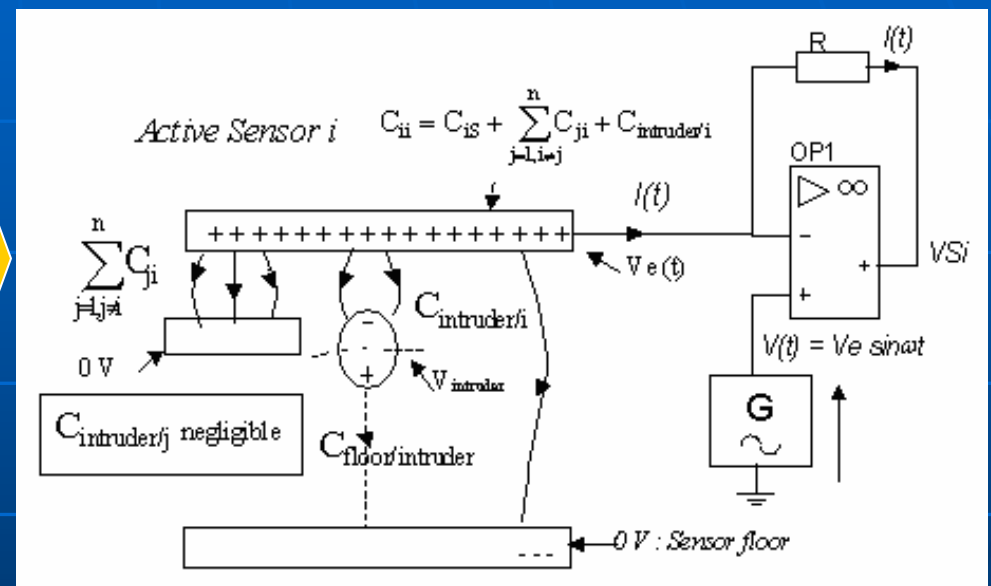
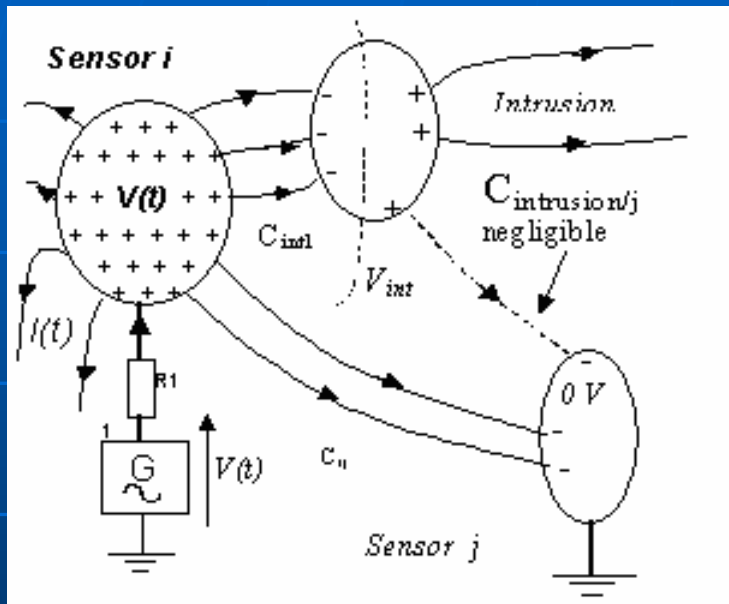


Localization and discrimination of the intruder

Design : Two identical sensors separated by Δd

II. Detection and Discrimination Set-up: DETECTION OF AN INTRUDER AND VALIDATION (1/3)

A. The intruder is **not in contact** with the floor (far enough), this latter behaves like a 'sensor j' at a null potential



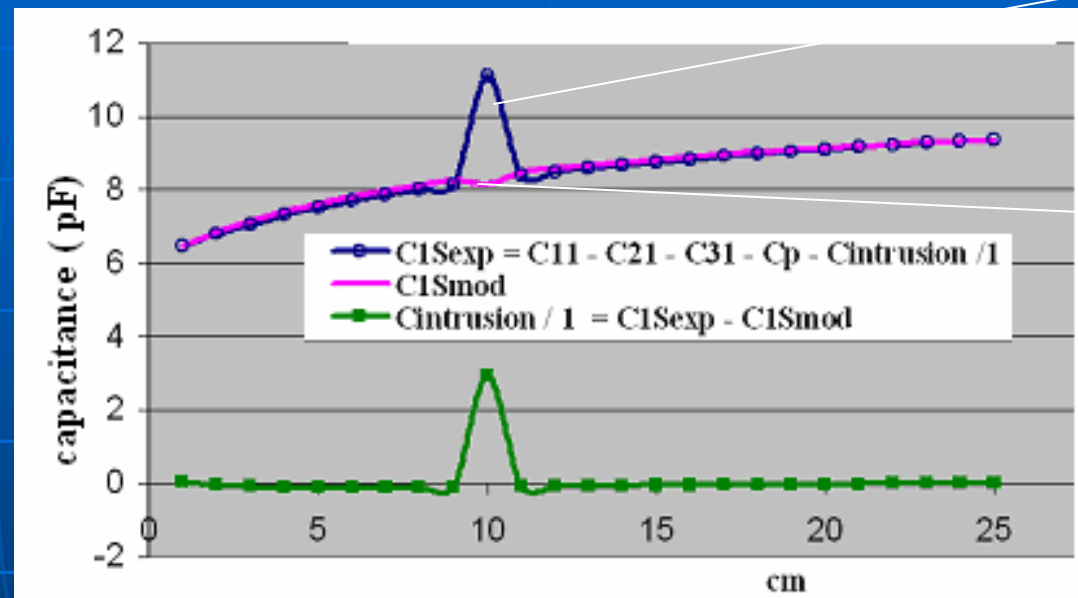
$$V_{Si} = V_e \sqrt{1 + (R\omega)^2 [C_{iS} + \sum_{j=1, i \neq j}^n C_{ji} + C_{intruder/i}]^2}$$

$$\sum_{j=1, i \neq j}^n V_{Sj} = V_e \cdot R\omega [\sum_{j=1, i \neq j}^n C_{ij} + C_{intruder/j}] \approx V_e R\omega \sum_{j=1, i \neq j}^n C_{ij}$$



$$C_{intruder/i} = C_{iS} (\dots)_{exp} - C_{iS} (\dots)_{model}$$

II Detection and Discrimination Set-up : DETECTION OF AN INTRUDER AND VALIDATION (2/3)



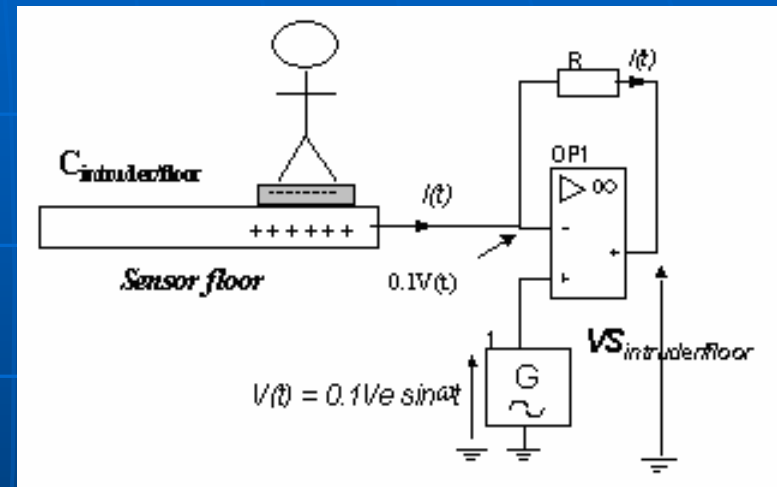
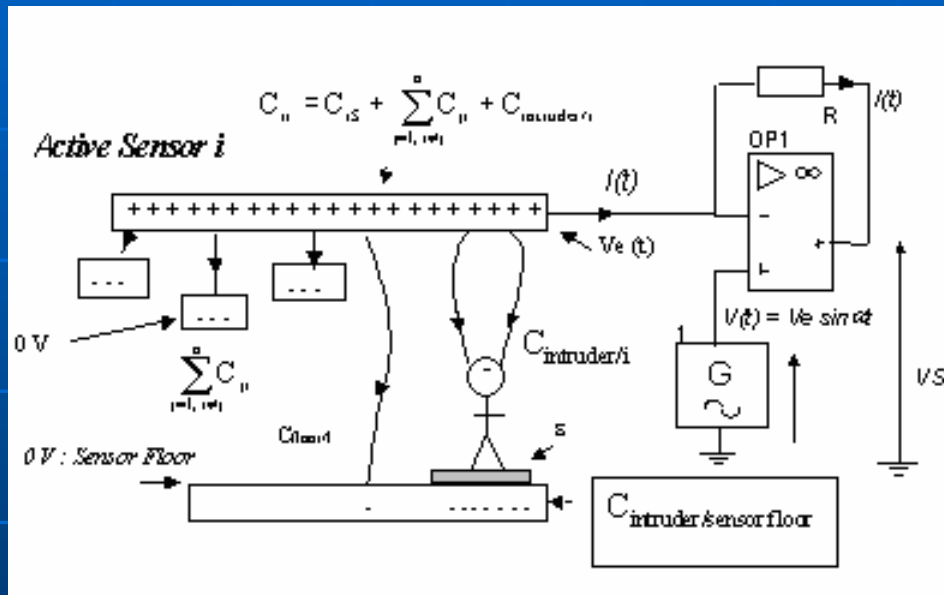
By measuring
the potential at
the output of the
circuit

Reference
model

Presence of a human being 10 cm away from an active sensor

II Detection and Discrimination Set-up : DETECTION OF AN INTRUDER AND VALIDATION (3/3)

B. The intruder is in contact with the floor, the capacitive coupling intruder/floor is not negligible.



Coupling intruder/floor

Detection of an intruder with the floor

$$V_{Si} = V_e \sqrt{1 + (R\omega)^2 [C_{iS} + \sum_{j=1, j \neq i}^n C_{ji} + C_{intruder/i} - C_{intruder/floor}]^2}$$

$$V_{Sintruder} = V_e \cdot R\omega [C_{intruder/floor}]$$

$$C_{intruder/i} = C_{iS}(\dots)_{exp} - C_{iS}(\dots)_{mod} - C_{intruder/floor}$$